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CHEN Hongkai, ZHANG Bin, WANG Shengjuan, et al. Study of the "roasted pigskin-effect" of post-fire debris flow[J]. Journal of Soil and Water Conservation, 2025, 39(3):345-351.

# 火后泥石流烧猪皮效应

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摘 要:[目的]火后泥石流是一种具有普遍共性特征的特殊泥石流类型,起源于大型及特大型森林火灾。发现火后泥石流存在烧猪皮效应,其核心是山火对下垫面植被及岩土介质的火煅作用。[方法]采用数值模拟方法分析下垫面火煅作用,揭示山火灾害发生后下垫面温度传导过程及温度应力变化规律。[结果]山火对下垫面的影响深度可达到3m,温度应力可达到405 MPa,易使下垫面岩土体发生热裂分解;提出火后物源概念,建立火后物源结构模型,包括火山灰烬层和火煅层2部分,前者是火后泥石流初期的主要物源,后者是火后泥石流中后期的主要物源。基于火后物源,探讨火后泥石流形成机理,即针对灰烬物源的面洗演化阶段和针对火煅层的沟蚀演化阶段,前者出现在山火后2 a左右时间内,后者出现的时间跨度大,可及千年至万年时间尺度;从火后泥石流烧猪皮效应角度,探讨开展火后泥石流防治思路问题。[结论]研究成果对于火后泥石流形成机制研究及靶向治理有积极意义。

关键词:火后泥石流;烧猪皮效应;下垫面火煅作用;火后物源;火后泥石流发育机理

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# Study of the "Roasted Pigskin-Effect" of Post-Fire Debris Flow

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Abstract: [Objective] Post-fire debris flow is a specific type of debris flow with universal common characteristics, originating from large forest fires. It is found that there is a "roasted pigskin effect" in post-fire debris flows, which is primarily attributed to the fire-calcined effect of wildfires on the underlying surface vegetation and rock-soil media. [Methods] Numerical simulation was used to analyze the fire-calcination effect on the underlying surface and reveal the temperature conduction process and changes of temperature stress on the underlying surface following the wildfire disaster. [Results] The depth of influence of wildfire on the underlying surface could reach 3 m, and the temperature stress could reach 405 MPa, which could easily cause thermal cracking and decomposition of the underlying rock and soil. The concept of the post-fire material sources was proposed, and a structure model of the post-fire material sources was established, which included two parts, namely, the volcanic ash layer and the fire-calcined layer, with the former being the primary source of the initial stage of post-fire debris flow, and the latter being the primary source of the mid-and late-stage of the post-fire debris flow. Based on the post-fire material sources, the mechanism of post-fire debris flow formation was explored, i.e., the stage of surface-washing evolution for ash material sources and the stage of gully erosion evolution for the fire-calcined layer, the former appeared in about two years after the wildfire, while the latter spanned a much longer time scale, potentially reaching millennium

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**Keywords**: post-fire debris flow; the roasted pigskin effect; fire-calcination effect on the underlying surface; post-fire material sources; development mechanism of the post-fire debris flow

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山火,又称森林火灾,是一种发生在林野的火 情,通常由高温、连续干旱、大风等天气条件变化引 起,也可能由人类的粗心大意或故意纵火所致。如 2019年1月7日15:00,四川省甘孜藏族自治州九龙县 子耳乡发生森林火灾,火场海拔高度1600~3200 m, 过火面积约0.4 km²;2020年3月30日15:51,四川省凉 山彝族自治州经久乡马鞍村发生森林大火,瞬间风向 突变,造成专业扑火队员18人牺牲。火烧迹地,下垫 面物理力学特性发生显著变化,易于在强降雨及冰 雪融水作用下发生泥石流灾害,WELLS称之为火后 泥石流,并指出火后泥石流比常规泥石流更易起 动[1],胡卸文等[2]研究发现,70%的林火后都发生泥 石流灾害。在火后泥石流研究中,以灰烬为代表的 火烧产物为泥石流提供更多物源,已经形成共识[3-9]。 已有研究[10-17]着眼于火烧迹地灰烬及高温破坏土 壤团聚体,研究火后泥石流形成机理、物源启动 模式、物源动储量估算,更多的是强调灰烬及表层 土体对强降雨的响应问题,与 DIBIASE 等[18]、 AALEXANDER 等[19]、STALEY 等[20]和 GUILINGER 等[21]的研究思路基本相同。部分学者从山火对地 表土壤的物理力学特性变化及产沙量角度研究火 后泥石流成因机制,如FELLING等[22]对美国加州-内华达州典型火烧迹地研究发现,火灾后土壤饱和 水力传导率降低200%,火灾会放大降雨径流, ROBICHAUD等[23]发现,火灾后第1a最高产沙量最 大。综上,总体看来,目前对火后泥石流的研究聚焦度 还不够,尤其未对山火对地表岩土层高温煅烧作用进 行深入研究。据统计[24],2000—2018年发生山火灾害 129 840次,其中大型及特大型火灾占42%,火场面积 计3.78万km<sup>2</sup>。森林火灾地表火温一般400℃、树冠火 达到900℃,在美国加利福尼亚甚至可达到1200℃。 生活常识告诉我们,带皮猪肉都有烧猪皮环节,目的是 清除皮囊里的污染油脂和残留断毛,使猪肉易于炖煮 和去腥营养,其科学原理是表层介质的热力崩解与碳 化。由此推知,山火对下垫面岩土介质必然存在火煅 作用,其火煅后效应称为烧猪皮效应。本文通过下垫 面火煅作用模拟,研究火后物源问题,据此分析火后泥

石流形成机制,对于深入开展火后泥石流形成机制研究及靶向治理有积极意义。

### 1 材料与方法

借鉴石灰和水泥煅烧原理,山火发生后下垫面岩土介质必然存在高温裂解问题。构建下垫面火煅作用模式(图1),即:强大、持续的山火使地表高温向下垫面深层传导,煅烧下垫面表层树根及岩土体,把高温向下传导的前沿边界称为煅烧锋。随着山火强度增强、历时延长,煅烧锋从地表逐渐向下垫面深层扩展。煅烧锋上部火煅层范围内的岩土介质存在火煅致裂问题,采用数值模拟方法分析下垫面火煅作用。

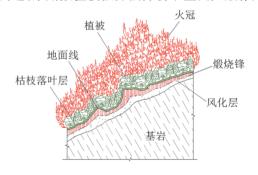


图 1 下垫面火煅作用概化模型

Fig. 1 Generalized model for the fire-calcination effect on the underlying surface

将计算模型导入 ABAQUS/CAE 软件中,模型内部传热模型视为沿着坡面法向一维传热。定义风化层和基岩体材料属性,采用自由网格划分技术划分网格模型,建立模型尺寸为50 m×70 m×50 m(图2)。设置模型的初始温度为20℃,创建后续分析步,编辑相互作用。在模型中假设坡体为各向同性弹性体,按照第 I类边界条件施加边界温度条件。上部温度边界为给定温度边界条件,底部及周围为自由边界条件。模拟过程中不考虑岩土介质的自重应力。根据火灾全过程中火灾的形成及衰退现象,采用升温(火灾初期)、恒温(全盛时期)、降温过程(衰退时期)进行模拟。由于目前尚未见森林火灾升温曲线的报道,本文采用国际标准组织(ISO)理论实验曲线(图3),确定升温过程温度曲线,见公式(1)。设置全过程起始温度 20℃,结束温度 50℃,总时间历程 720

min;其中,火烧升温过程持续120 min(0~2 h),恒温 过程持续120 min(2~4 h),降温过程持续480 min (4~12 h)。由公式(1)计算得知,全程最高温度为1

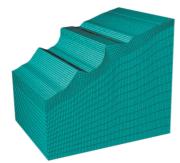


图 2 下垫面火煅作用有限元模型

Fig. 2 A FEM model for the fire-calcination effect on the underlying surface

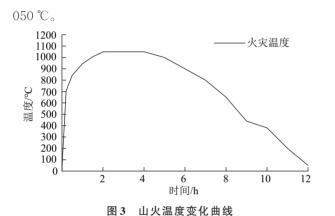


Fig. 3 Temperature variation curve of the wildfire

 $T - T_0 = 345 \log_{10}(8t + 1)$ (1)

式中:t为火烧经历时间, $\mathbb{C}$ :T为最终温度, $\mathbb{C}$ :T。为 初始温度,℃。

下垫面火煅作用模拟相关参数见表1。

# 结果与分析

#### 2.1 下垫面温度传导过程

由图 4 可知, 山火发生后, 初期 2~3 h, 下垫面表 层温度上升迅速,集中在下垫面表层;山火升温过程 中,下垫面温度快速上升并向深部岩土层传导,表层 温度变化于80~1050℃;山火恒温过程中,煅烧锋快 速向下垫面深层推进;山火降温过程中,下垫面岩土 体内部积聚大量热量且消散较慢,内部仍存在较高 温度,温度远大于坡体表面,煅烧锋继续向深部推 进,且不同微地貌部位,煅烧锋推进深度存在显著差 异。由图5可知,在山火发生2h内,煅烧锋可快速推 进到深度 0.6~1.0 m, 随后进入缓慢准线性增大阶 段。升温过程最大影响深度为2.9 m,火烧12 h影响 平均深度为3.29 m。图6为下垫面0、1、2、3 m深度 位置的温度变化曲线。可见,埋深越大温度变化幅 度越小,温度增幅在升温阶段最大。埋深1~2 m处 岩土介质受温度影响较大,埋深1m时温度最大点出 现在火烧4~6h(降温阶段),埋深2m时温度最大点 出现在8~10 h(降温阶段),埋深3m时受温度影响 较小,温度增幅变化不大。

表 1 下垫面火煅作用模拟相关参数

Table 1 Parameters of the model of the fire-calcination effect on the underlying surface

Tubic 1 Turum certs of the model of the fire culcination effect on the underlying surface						
类型	密度/(kg·m <sup>-3</sup> )	泊松比	弹性模量/MPa	热传导率/ (W·m <sup>-1</sup> ·K <sup>-1</sup> )	比热/ (J•kg <sup>-1</sup> •K <sup>-1</sup> )	热膨胀系数/K-1
风化层	1 800	0.30	20	3.30	400	$10^{-4}$
基岩	2 000	0.28	34 500	2.55	970	$10^{-4}$
(a) 0.5 h	NT11  1.974e+0.7  1.974e+0.7	(b) 6 h	NT11  9.463e+02  8.63e+02  -7.63e+02  -7.07e+02  -4.70e+02  -4.70e+02  -3.14e+02  -2.36e+02  -7.88e+01	(c) 8 h	NT11 1,049e+03 2,049e+03 3,049e+02 3,65e+02 3,65e+02 6,04e+02 4,371e+02 4,371e+02 7,672e+02 7,672e+03 8,742e+01	NT11
(e) 8 h	NT11 -6.694e+02 -6.136e+02 -6.136e+02 -5.020e+02 -3.905e+02 -3.905e+02 -3.347e+02 -7.334e+02 -1.116e+02 -5.578e+01	(f) 10 h	NT11  -5.063e+02 -4.643e+02 -4.643e+02 -3.798e+02 -3.798e+02 -2.532e+02 -2.110e+02 -2.110e+02 -1.188e+03 -8.439e+01 -4.220e+01	(g) 12 h	NT11 -3.756e+02 -3.443e+02 -3.150e+02 -3.150e+02 -2.504e+02 -2.191e+02 -1.578e+02 -1.578e+02 -0.390e+01 -6.260e+01 -3.130e+01	

图 4 下垫面火煅作用温度云图

Fig. 4 Temperature change cloud diagram of the fire-calcination effect on the underlying surface

#### 2.2 下垫面温度应力变化特性

力主要集中在表层区域,最大温度应力由58 MPa增 由图7可知,山火升温阶段下垫面火煅层温度应 加至151 MPa。恒温阶段,温度向下垫面深部传导,

温度应力逐渐增大,12 h时可及 405 MPa,足可以使一般岩土体发生热裂分解。

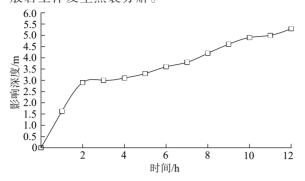


图 5 煅烧峰平均深度-时间关系

Fig. 5 Curve of the relationship between the average depth and duration of the calcination front

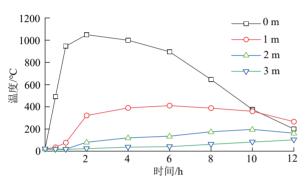


图 6 风化层深度-温度-时间关系

Fig. 6 Curves of the depth-temperature-duration relationships for the weathering zone

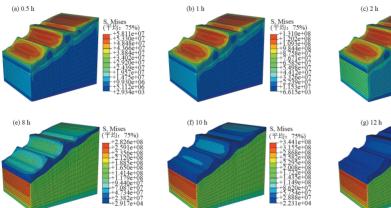


图 7 下垫面火煅层温度应力变化

Fig. 7 Temperature stress change cloud diagram of the fire calcination model of the underlying surface

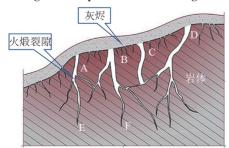


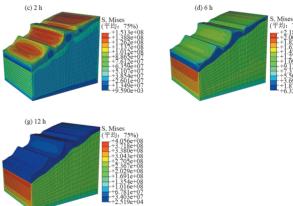
图 8 火后物源结构

Fig. 8 Pattern of post-fire materials causing debris flow

# 3 讨论

#### 3.1 关于火后泥石流形成机制

物源是形成泥石流的三大要素之一,一般是沟 谷或斜坡表层的松散岩土体及全强风化带,近年来 强震区把震裂山体表层也归并到泥石流物源,提出 物源动储量问题[25];陈洪凯等[26]基于现场勘测和有 限元模拟,提出泥石流沟物源稳定性分区方法,指出 根据不稳定和极不稳定物源区确定泥石流物源储 量。然而,由山火引发的火后泥石流物源具有特殊 的共性特征,即初期物源为山火灰烬层,后期是下垫 面火煅层,统称为火后物源。由构建火后物源结构 (图8)可知,灰烬层在降雨冲击和径流洗刷作用下易 于失稳流动,成为火后泥石流初期物源;同时,灰烬 层物源启动后,部分饱和及非饱和灰烬浆体对火煅 裂隙顶部A、B、C、D端口有阻塞作用,地表径流入渗 火煅层少,加强灰烬层的面洗作用;灰烬层冲蚀殆尽 后,A、B、C、D端口逐渐开启,进入火煅裂隙的残余 灰烬浆体及地表径流,在裂隙网络内产生静水压力 并软化裂隙洞壁岩土介质,出现潜蚀作用,加速火煅 层裂解,成为火后泥石流后期物源。在地表比较陡 峻的部位,2~3 m的火煅层在潜蚀作用下易于发生 表层岩土体剥离与流滑,表现为土溜及群发性小 滑坡。



火后泥石流研究,应该抓住火后物源这一关键环节,从火后物源的启动问题着手研究火后泥石流形成机制问题。据此思路,火后泥石流发育存在2个阶段:

1) 面洗演化阶段 山火灾害出现后,产生灰烬物源,在强降雨或冰雪融水作用下,灰烬层产生多个局部饱和区,局部饱和区逐渐归并,以坡面冲刷方式启动,形成广布火烧迹地的坡面泥石流(图9)→大量的坡面泥石流汇集到山坡坡麓或沟谷内,形成沟谷泥石流。

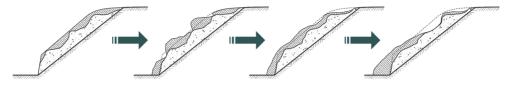


图 9 火后泥石流初期的坡面泥石流演化模式

Fig. 9 Evolution pattern of slope debris flow at the early stages of a post-fire debris flow

该阶段是目前大部分学者研究火后泥石流最关 心的问题,如MOODY等[27]研究发现,火灾过后土壤 的抗冲刷能力下降,并存在灰烬层,面对显著增大的 坡面径流,泥石流启动的降雨阈值显著降低;黄健 等[11]在探讨四川西昌"3·30"响水沟火后泥石流成灾 机理时,降雨阈值最小为5.4 mm/h,明显低于该区域 5年一遇的降雨强度;吉日伍呷等[28]研究发现,凉山 州喜德境内火后泥石流暴发所需的降雨阈值急剧降 低,10 min 及1h降雨阈值分别降低55.62%与 76.62%。显然,此阶段并不能完全代替火后泥石流 全过程发育机制问题,"火后泥石流降雨阈值显著降 低"并不是一个共性规律,只适用于火后泥石流初期 的泥石流灾害预测预警,在下垫面灰烬物源消失殆 尽后,该观点便不再正确。MCGUIRE等[9]已经认识 到该问题,指出山火发生1a内,泥石流15 min降雨量 阈值为15~30 mm/h,第3 a则增加到60 mm/h。由于 灰烬物源存留时间短,一般3~5场暴雨便可冲蚀 80% 左右,2 a左右基本消失,进一步研究中,必须转 变泥石流研究传统思路:一是采用现场勘测与室内 模拟试验相结合,深入开展火后物源研究,构建火后 物源储量确定方法,研究火后物源释放方式、机理及 速率;二是综合考虑引发泥石流的降雨阈值与火后物 源的关联性,探讨火后泥石流动态降雨阈值问题,彻 底厘清"火后泥石流降雨阈值会显著降低"的观点。

2) 沟蚀演化阶段 灰烬物源基本耗散完毕后,火煅裂隙网络地表开口端(图8中A、B、C、D处)开启,大量地表径流进入火煅裂隙内,火煅层在入渗水体的潜蚀作用下,在边坡表层产生强烈沟道侵蚀作用,引发群发性地表滑塌体、小型滑坡,汇集到沟谷,形成规模较大的沟谷泥石流。由于火煅层物源则存留时间长,甚至可达到千年及万年时间尺度,进一步研究,应采用地貌侵蚀理论研究该阶段泥石流发育问题,尤其需要采用岩土力学方法研究火煅物源的稳定性及其起动问题。

### 3.2 关于火后泥石流防治问题

不同学科对泥石流灾害防治侧重点存在差异, 水土保持领域强调泥石流全流域综合防控,监测预警与工程治理相结合,控源、拦挡、排导、淤积,多技术综合应用;在公路、铁路交通领域,陈洪凯提出"礼 让出境"公路泥石流防治新思路,将泥石流体从道路内侧有效排泄到道路外侧深沟或河道内,保障道路挡防结构安全及交通运输营运安全[29]。而防控火后泥石流灾害,应该以烧猪皮效应理论为指导,客观面对火后物源,尤其应将火后泥石流视为局部文明,重视灰烬物源土壤肥力加速迁移及存储问题,研发稳固火煅层、拦挡枯枝滚石、灰烬水流沉淀固肥、山洪排泄等新技术新方法,构建"控源-拦挡-淤沉-排导"综合防控技术体系。

### 4 结论

1)发现火后泥石流存在烧猪皮效应,其核心是山火对下垫面植被及岩土介质的火煅作用。数值模拟表明,山火对下垫面的影响深度可达到3m,温度应力可达到405 MPa,易使下垫面岩土体发生热裂分解。

2)火后泥石流形成机理研究应该从火后物源失稳启动着手,包括针对灰烬物源的面洗演化阶段和针对火煅层的沟蚀演化阶段,前者出现在山火后2a左右时间内,后者出现的时间跨度大,可及千年至万年时间尺度。

3)从火后泥石流烧猪皮效应角度,探讨开展火后泥石流防治思路问题,重视灰烬物源土壤肥力加速迁移及存储问题,研发稳固火煅层、拦挡枯枝滚石、灰烬水流沉淀固肥、山洪排泄等新技术新方法,构建"控源-拦挡-淤沉-排导"综合防控技术体系。

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